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# RETURN PERIOD ANALYSIS AS A TOOL FOR URBAN FLOOD PREDICTION IN THE NIGER DELTA: A CASE STUDY OF PORT HARCOURT CITY, NIGERIA 

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#### Abstract

The study examined return period analysis as a tool for flood prediction in urban areas. This technique enables us to know when an event is expected to occur, be equaled, or be exceeded. When floods occur, the effects are always very devastating, sometimes resulting in destruction of homes, villages, human life and property. Urban floods in most cases result from unplanned, uncoordinated urbanization projects, poor sanitary habits of dumping of refuse, and poorly maintained and insufficient drainage. These are well highlighted in this study. Results indicate that for thirty years of data, the return period is 10.3 years for a maximum 1-month rainfall of 804 mm with a maximum 1-year rainfall of $2,544 \mathrm{~mm}$ for same return period. The study recommends routing through specific drainages in flood prone areas of Port Harcourt to mitigate the impacts of flooding.


## INTRODUCTION

The Niger Delta area is located in the most southerly part of Nigeria. It is one of the world's largest wetlands with a total land area of approximately $29,000 \mathrm{~km}^{2}$ excluding the continental shelf (NDES, 1997). Port Harcourt, the capital of Rivers State with a population of about 1,356,000 (Federal Office of Statistics, 2003) is a major industrial city in the Niger Delta region (FEPA/ World Bank, 1998).

Port Harcourt suffers from urban flooding as a result of insufficient drainage capacity, and uncoordinated and poorly maintained drainages. The situation is worsened because of unplanned urbanization patterns leading to blockage of existing drainages, rapid population explosion and poor sanitary habits as a result of dumping volumes of refuse in gutters, drainage outlets and adjoining creeks (Ayotamuno and Gobo, 2004).

A direct consequence of the expansion in the built-up area is the increase in the extent of impervious surfaces which also increases surface runoff, causing floods in the city. Added to these effects are the indiscriminate canalization and the attendant creation of ingress channels for flood waters.

Human activities also aggravate flooding in urban cities. According to Akintola (1978) and Odemerho (1988), it is generally believed that urbanization, particularly when it encroaches on areas which were once farmlands or forests, causes the most remarkable flood-intensifying land use change. The removal of natural vegetation cover from a forested area during construction work can lower the infiltration capacity to a point where rainfall intensity significantly exceeds the water infiltration rate thereby causing floods (Dunne and Leopard, 1978). It is also argued that volume and timing of runoff are substantially modified by forest clearing.

Espey et al. (1966) found that the replacement of permeable by impervious surface through urbanization results in peak discharges which were from 100 to 300 per cent greater than those from undeveloped areas. Wolman and Schick (1967) and Alfesehi (1990) confirmed that changes in the urban landscape which aggravated flows have not only increased surface runoff but also sediment load in basins, along streets and storm channels resulting in change in channel morphology. Increases in urban floods are also related to building along runoff areas, impervious urban surfaces, inadequate storm drains and dumping of refuse in drains and drainage paths, uncoordinated physical development, and the absence of storm sewers.

The most useful approach to the prediction of flood flows is the statistical method of frequency analysis (Subramanya, 1991). This is because hydrologic processes such as floods are exceedingly complex natural events, and result from the interplay of a number of components/parameters that are very difficult to model analytically. For example, the floods in a catchment depend on rainfall and antecedent conditions, and each of these factors in turn depend upon a host of constituent parameters. Return period analysis becomes important because of its simplicity and ease of application. Return period values are important for designs of channels, bridges, culverts, waterways and spillways for dams and estimation of scour for hydraulic structures.

## STUDY AREA

Port Harcourt is located within latitudes $6^{\circ} 58^{\prime} \mathrm{N}$ to $7^{\circ} 6^{\prime} \mathrm{N}$ and Longitude $4^{\circ} 40^{\prime} \mathrm{E}$ to $4^{\circ} 55^{\prime} \mathrm{E}$ (Figure 1). It falls almost entirely within the lowland swamp forest ecological zone and is flanked in the east, west and southern limits by mangrove swamp forest (Braide et al., 2004; Chindah,
2004). Port Harcourt constitutes the second largest port in Nigeria in terms of tonnage handling. It also constitutes an important terminal for connection to the outlying villages in the delta area. As the capital of Rivers State, Port Harcourt has become an important administrative center with regular air connections to other parts of Nigeria.

The town is therefore an important industrial and commercial center. Access to cheap energy from oil and natural gas, in addition to good communications, have created favorable conditions for Port Harcourt to become Nigeria's most important industrial town. The area experiences heavy rainfall averaging $2500 \mathrm{~mm} /$ annum. It rains for about eight months (March to October) during the year, and even the months considered as dry months are not free from occasional rainfall (Gobo, 1990). It has an almost flat topography and is underlain by superficial soil that consist of silty clays mixed with silty sand. The water table is less than 10 m below ground surface. The combination of excessive rainfall, inadequate and poorly maintained drainages, and low permeability of the superficial soils dispose the area to flooding on an annual basis whenever rainfall is in excess of 100 mm .

In spite of its economic importance, the city experiences intermittent flooding in a large number of areas. Some of the most affected areas include:

1) Waterline Junction (by College of Education bus stop)
2) Olu Obasancjo Road (Police Station) by Omoku Street
3) Diobu (Mile Three Building Material area)
4) Diobu (Mile One Market area)


Figure 1. Map of the study area showing the geographical location of Port Harcourt
5) Amadi Flats (Nzimiro Street)
6) Amadi Flats (Herbert Marculey by Yola street)
7) Diobu (Education Bus Stop area)
8) Civic Centre by Hospital Road
9) Azikiwe by Industry Road
10) Superboard Bus Stop by First Bank
11) Port Harcourt Main Post Office by Central Bank
12) Station Bus Stop (Round About) by Hospital Road

The spatial distribution of these locations is shown in Figure 2.


Figure 2. Map of Port Harcourt Government Area showing areas prone to flooding.

## METHODOLOGY

The data include maximum daily rainfall data from 1975-2004 (30 years inclusive). This finds justification in climatologists adoption of the practice of forming climate change estimates from a thirty-year reference period (Miller, 1961). Maximum daily rainfall values were used since flood problems are always considered in terms of worst or extreme situations.

Recurrence predictions are often calculated in terms of return periods. The return period of a given event is the average number of years within which the event is expected to be equaled or exceeded (that is, the expected average frequency of occurrence of an event over a longer period of years) (WMO 1983).

The data are arranged in descending order and the probability $(\mathrm{P})$ and recurrence intervals of various events are calculated as indicated in the Tables 1 and 2 (Where $\mathrm{n}=30$ and $\mathrm{n}+1=31$ ).

Table 1. Maximum 1-month rainfall values (mm) for Port Harcourt [1975-2004] (30 Years inclusive).

| M | Year | Rainfall (RR) |  | $\mathrm{P}=\mathrm{m} / \mathrm{n}+1$ | $\mathrm{RT}=\frac{1}{p}$ | Log of RT | Log of Rainfall (RR) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2000 | 1036.011 | $1 / 31=$ | 0.032258 | 30.9981 | 1.4913 | 3.0154 |
| 2 | 1997 | 826.648 | 2/31 $=$ | 0.06452 | 15.4991 | 1.1903 | 2.9173 |
| 3 | 1998 | 803.727 | 3/31 $=$ | 0.09677 | 10.3338 | 1.0143 | 2.9051 |
| 4 | 1995 | 757.134 | 4/31 $=$ | 0.129 | 7.7519 | 0.8894 | 2.8792 |
| 5 | 1993 | 712.519 | 5/31 $=$ | 0.1613 | 6.1996 | 0.7924 | 2.8528 |
| 6 | 1979 | 701.3 | 6/31 $=$ | 0.1935 | 5.168 | 0.7133 | 2.8459 |
| 7 | 1994 | 680.043 | 7/31= | 0.2258 | 4.4287 | 0.6463 | 2.8325 |
| 8 | 1987 | 663.1 | 8/31 $=$ | 0.2581 | 3.8745 | 0.5882 | 2.8216 |
| 9 | 1992 | 645.892 | 9/31 $=$ | 0.2903 | 3.4447 | 0.5372 | 2.8102 |
| 10 | 1980 | 637.82 | 10/31 $=$ | 0.3226 | 3.0998 | 0.4913 | 2.8047 |
| 11 | 1975 | 622 | 11/31 $=$ | 0.3548 | 2.8185 | 0.4500 | 2.7938 |
| 12 | 1991 | 615.285 | 12/31 $=$ | 0.3871 | 2.5833 | 0.4122 | 2.7891 |
| 13 | 1977 | 607.64 | 13/31 $=$ | 0.4194 | 2.3844 | 0.3774 | 2.7836 |
| 14 | 2003 | 602.6 | 14/31 $=$ | 0.4516 | 2.2143 | 0.3452 | 2.7800 |
| 15 | 2002 | 596.9 | 15/31 $=$ | 0.4839 | 2.0665 | 0.3152 | 2.7759 |
| 16 | 1990 | 587.903 | 16/31 $=$ | 0.5161 | 1.9376 | 0.2873 | 2.7693 |
| 17 | 1988 | 576.61 | 17/31 $=$ | 0.5484 | 1.8235 | 0.2609 | 2.7609 |
| 18 | 1978 | 570.2 | 18/31 $=$ | 0.5806 | 1.7224 | 0.2361 | 2.7560 |
| 19 | 1981 | 566.9 | 19/31 $=$ | 0.6129 | 1.6316 | 0.2126 | 2.7535 |
| 20 | 1982 | 534 | 20/31 $=$ | 0.6452 | 1.55 | 0.1903 | 2.7275 |
| 21 | 1996 | 521.415 | 21/31 $=$ | 0.6774 | 1.4762 | 0.1691 | 2.7172 |
| 22 | 1984 | 520 | 22/31 $=$ | 0.7097 | 1.409 | 0.1489 | 2.7160 |
| 23 | 1986 | 519.6 | 23/31 $=$ | 0.7419 | 1.3479 | 0.1297 | 2.7157 |
| 24 | 2001 | 511.6 | 24/31 $=$ | 0.7742 | 1.2919 | 0.1112 | 2.7089 |
| 25 | 1976 | 508.4 | 25/31 $=$ | 0.8065 | 1.24 | 0.0934 | 2.7062 |
| 26 | 1999 | 507.913 | 26/31 $=$ | 0.8387 | 1.1923 | 0.0764 | 2.7058 |
| 27 | 1989 | 506.1 | 27/31 $=$ | 0.87096 | 1.1482 | 0.0600 | 2.7042 |
| 28 | 2004 | 469.3 | 28/31 $=$ | 0.9032 | 1.1072 | 0.0442 | 2.6715 |
| 29 | 1985 | 491.02 | 29/31 $=$ | 0.9355 | 1.0689 | 0.0289 | 2.6911 |
| 30 | 1983 | 382.2 | 30/31 $=$ | 0.9677 | 1.0334 | 0.0143 | 2.5823 |
| Total |  | 18281.78 |  | 14.9999 | 123.8453 | 12.3174 | 83.2932 |

Table 2. Maximum yearly (1-year) rainfall values (mm) for Port Harcourt [1975-2004] (30years inclusive)

| M | Year | Rainfall (RR) |  | $\mathrm{P}=\mathrm{m} / \mathrm{n}+1$ | $\mathrm{RT}=\frac{1}{p}$ | Log of RT | Log of Rainfall (RR) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1998 | 2569.3 | $1 / 31=$ | 0.03226 | 30.9981 | 1.4913 | 3.4098 |
| 2 | 1995 | 2569.3 | $2 / 31=$ | 0.06452 | 15.4991 | 1.1903 | 3.4098 |
| 3 | 1980 | 2544.9 | $3 / 31=$ | 0.09677 | 10.3338 | 1.0143 | 3.4057 |
| 4 | 1993 | 2542.4 | 4/31 = | 0.129 | 7.7519 | 0.8894 | 3.4052 |
| 5 | 1999 | 2499.6 | 5/31 $=$ | 0.1613 | 6.1996 | 0.7924 | 3.3979 |
| 6 | 1975 | 2491.5 | 6/31 $=$ | 0.1935 | 5.168 | 0.7133 | 3.3965 |
| 7 | 1988 | 2420.9 | 7/31 = | 0.2258 | 4.4287 | 0.6463 | 3.3840 |
| 8 | 2003 | 2407.7 | 8/31 $=$ | 0.2581 | 3.8745 | 0.5882 | 3.3816 |
| 9 | 1985 | 2395.6 | 9/31 $=$ | 0.2903 | 3.4447 | 0.5372 | 3.3794 |
| 10 | 1994 | 2374.2 | 10/31= | 0.3226 | 0.0998 | 0.4913 | 3.3755 |
| 11 | 1979 | 2342.5 | 11/31= | 0.3548 | 2.8185 | 0.4500 | 3.3697 |
| 12 | 1996 | 2339.4 | 12/31= | 0.3871 | 2.5833 | 0.4122 | 3.3691 |
| 13 | 1997 | 2329.4 | 13/31= | 0.4194 | 2.3844 | 0.3774 | 3.3672 |
| 14 | 1976 | 2321.8 | 14/31= | 0.4516 | 2.2143 | 0.3452 | 3.3658 |
| 15 | 1978 | 2291.2 | 15/31= | 0.4839 | 2.0665 | 0.3152 | 3.3601 |
| 16 | 1986 | 2283.1 | 16/31= | 0.5161 | 1.9376 | 0.2873 | 3.3585 |
| 17 | 1978 | 2261.3 | 17/31= | 0.5484 | 1.8235 | 0.2609 | 3.3544 |
| 18 | 1977 | 2235.5 | 18/31= | 0.5806 | 1.7224 | 0.2361 | 3.3494 |
| 19 | 2002 | 2166.2 | 19/31= | 0.6129 | 1.6316 | 0.2126 | 3.3357 |
| 20 | 1989 | 2160.2 | 20/31= | 0.6452 | 1.55 | 0.1903 | 3.3345 |
| 21 | 1981 | 2158.3 | 21/31= | 0.6774 | 1.4762 | 0.1691 | 3.3341 |
| 22 | 2001 | 2153.5 | 22/31 $=$ | 0.7097 | 1.409 | 0.1489 | 3.3331 |
| 23 | 1984 | 2126.8 | 23/31= | 0.7419 | 1.3479 | 0.1297 | 3.3277 |
| 24 | 1991 | 2094.4 | 24/31 = | 0.7742 | 1.2919 | 0.1112 | 3.3211 |
| 25 | 1990 | 2073.3 | 25/31= | 0.8065 | 1.24 | 0.0934 | 3.3167 |
| 26 | 2000 | 2068.9 | 26/31= | 0.8387 | 1.1923 | 0.0764 | 3.3157 |
| 27 | 1982 | 1991.5 | 27/31= | 0.8709 | 1.1482 | 0.0600 | 3.2992 |
| 28 | 1992 | 1962.2 | 28/31= | 0.9032 | 1.1072 | 0.0442 | 3.2927 |
| 29 | 2004 | 1877.5 | 29/31 $=$ | 0.9355 | 1.0689 | 0.0289 | 3.2736 |
| 30 | 1983 | 1632 | 30/31= | 0.9677 | 1.0334 | 0.0143 | 3.2127 |
| Total |  | 67684.4 |  | 14.9999 | 90.8453 | 9.3331 | 100.5364 |

## RESULTS AND DISCUSSION

Table 1 and Figure 3 give the return period for a maximum total 1-month rainfall (mm) using values from 1975 to 2004 (30 years inclusive) for Port Harcourt. The results indicate that the period is 15.5 years to obtain maximum 1-month rainfall $(\mathrm{mm})$ value of 826 mm . Furthermore, the results suggest that the period is 2.0 years for maximum 1-month rainfall (mm) of 587 mm to occur while a maximum 1-month rainfall ( mm ) of 382 mm could occur every year. These relationships can be numerically expressed as $y=0.2229 x+2.6849$ with a coefficient of determination of $R^{2}$ $=0.9250$. Table 2 presents maximum yearly rainfall in Port Harcourt. The return period


Figure 3. Return Period for maximum 1-month rainfall for Port Harcourt.
computation based on the annual maximum rainfall is presented in Figure 4. As regards Table 2 and Figure 4, it will take 10.3 years for maximum 1-year rainfall (mm) of $2,544 \mathrm{~mm}$ to occur. Furthermore, to obtain maximum 1-year rainfall (mm) of $2,291 \mathrm{~mm}$, it will take 2.1 years while the value of $1,166 \mathrm{~mm}$ rainfall could be obtained in every year. The regression equation for this relationship is: $y=0.0995 x+3.3104$ with $R^{2}=0.6747$. The coefficient of determination, $R^{2}$, indicates the strength of the relationship.

These values give the threshold or critical values that must be obtained and used for engineering designs for flood control works in Port Harcourt and its environs. Also Figure 2 shows that the Northwesterly (NW) through the Southwesterly (SW) sides of Port Harcourt lie at lower elevations and are more prone to flooding than the Northeasterly (NE), through the Southeasterly (SE) axes. The Trans-Amadi Axis (Figure 2) also suggests that drainages around the areas marked numbers (1) to (7) should be constructed and channeled into Abonnema Wharf Creek; while for the areas labeled (8) to (12) drainage should be constructed to run through the Eastern Bye Pass, through NEPA waterside, and into the Amadi-Amd/Abuloma Town Creeks.

## CONCLUSION AND RECOMMENDATION

This study has highlighted the need for basic statistical analysis of hydrometeorological data and application of the results for engineering design works to achieve desired flood control objectives. The results indicate that the return period is 15.5 years for maximum 1-month rainfall of 826 mm and maximum 1-year rainfall of 2569 mm to occur. In this era of frequent collapse of bridges, houses, dams and drainages as result of improper design, it is necessary for engineers to take all necessary statistical inputs into design process for effective works. Various routes and channels through which flood drainages could be channeled are also recommended.


Figure 4. Return Period for maximum 1-year rainfall for Port Harcourt.

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